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Introduction – Geotransfer factor

Knowing the environment

Ground water modelling

- Local Model
- Site Model
- Wetland model

Conclusions & Future work



# INTRODUCTION: GeoTransfer Factor

# Why do we need a Geo Transfer factor (GTF)

- To estimate the radiological impact of the disposal
- **Definition:** The ratio of the RN concentration in a biosphere receptor to the RN flux from disposal facility
- Higher GTF means there is a lower dilution in the geosphere
- Different biosphere receptors (pathways):
  - Private well
  - Wetlands

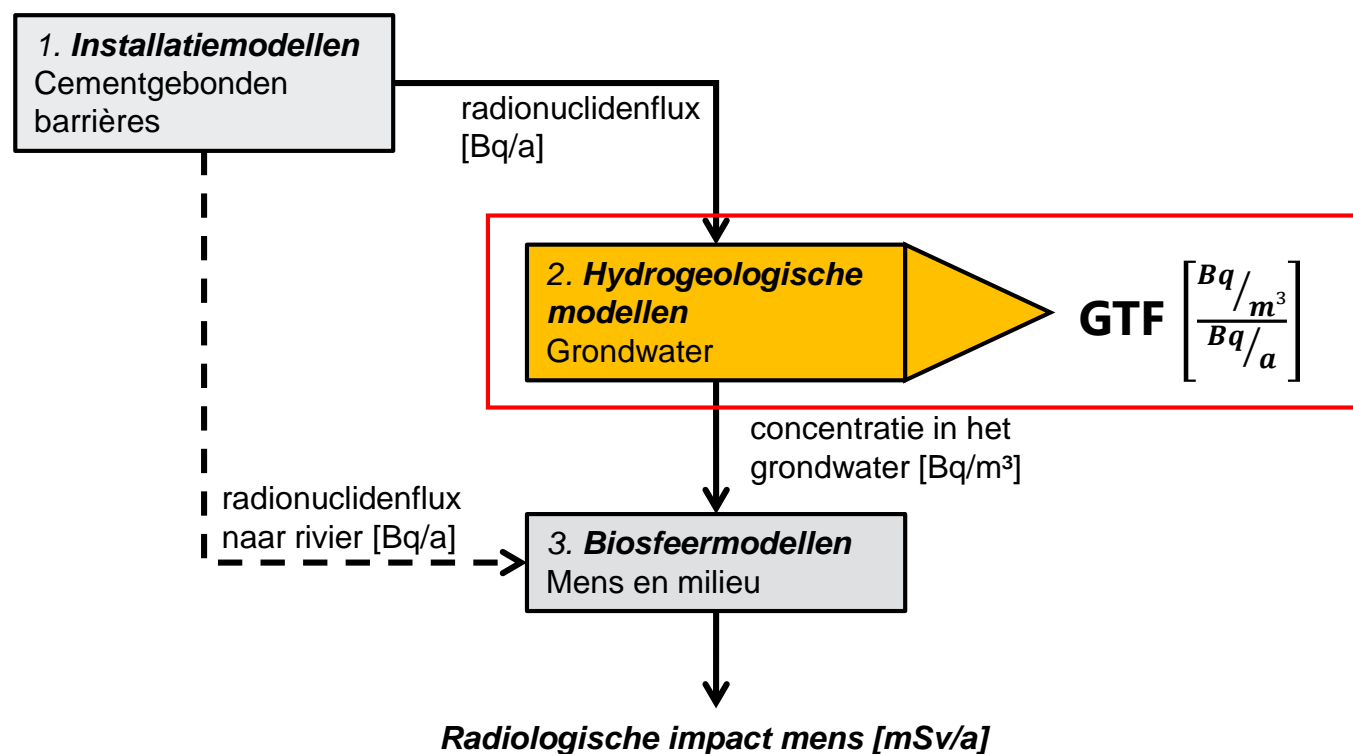
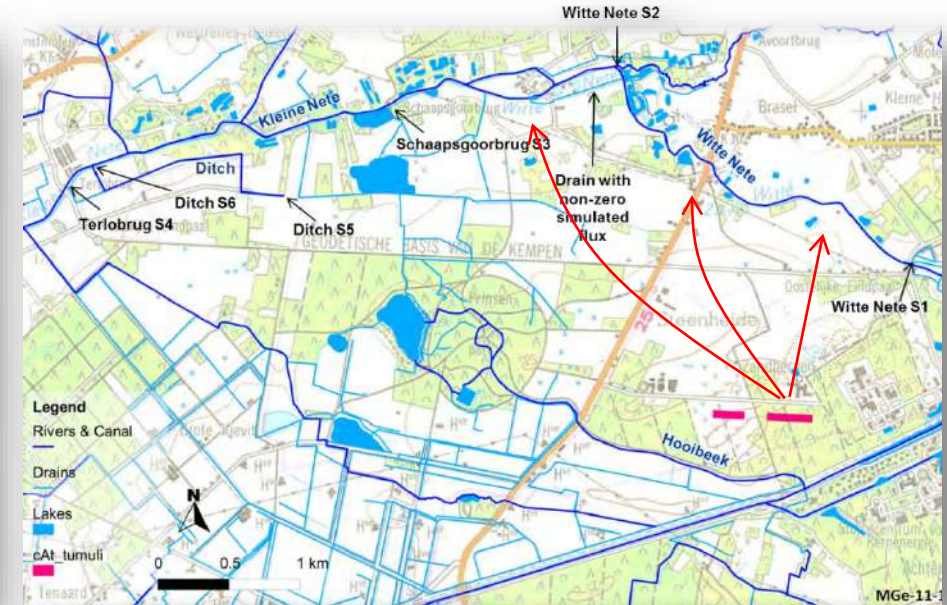
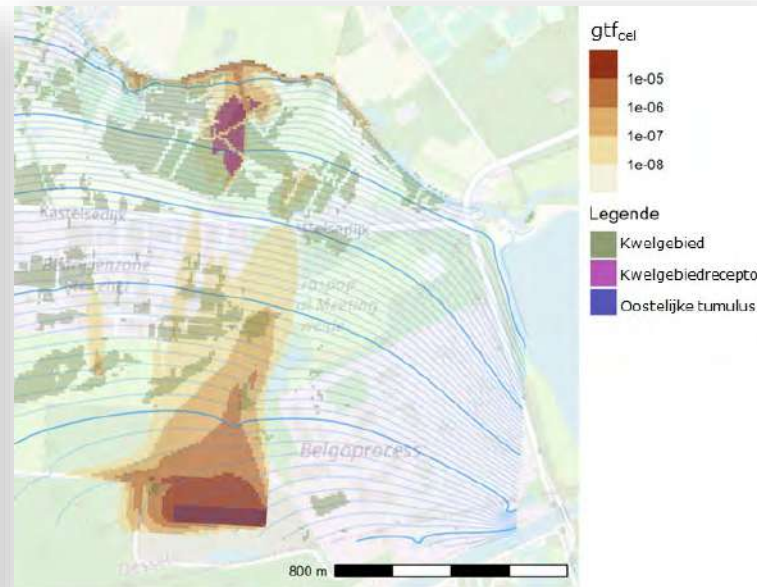
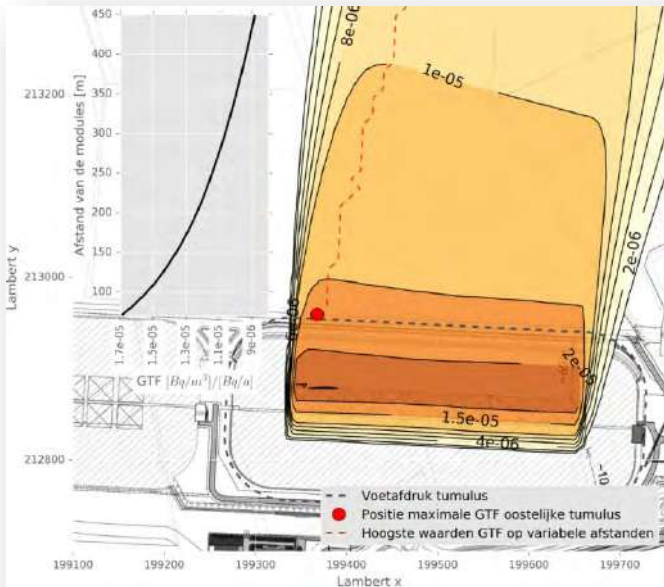


Figure adapted from the Safety file

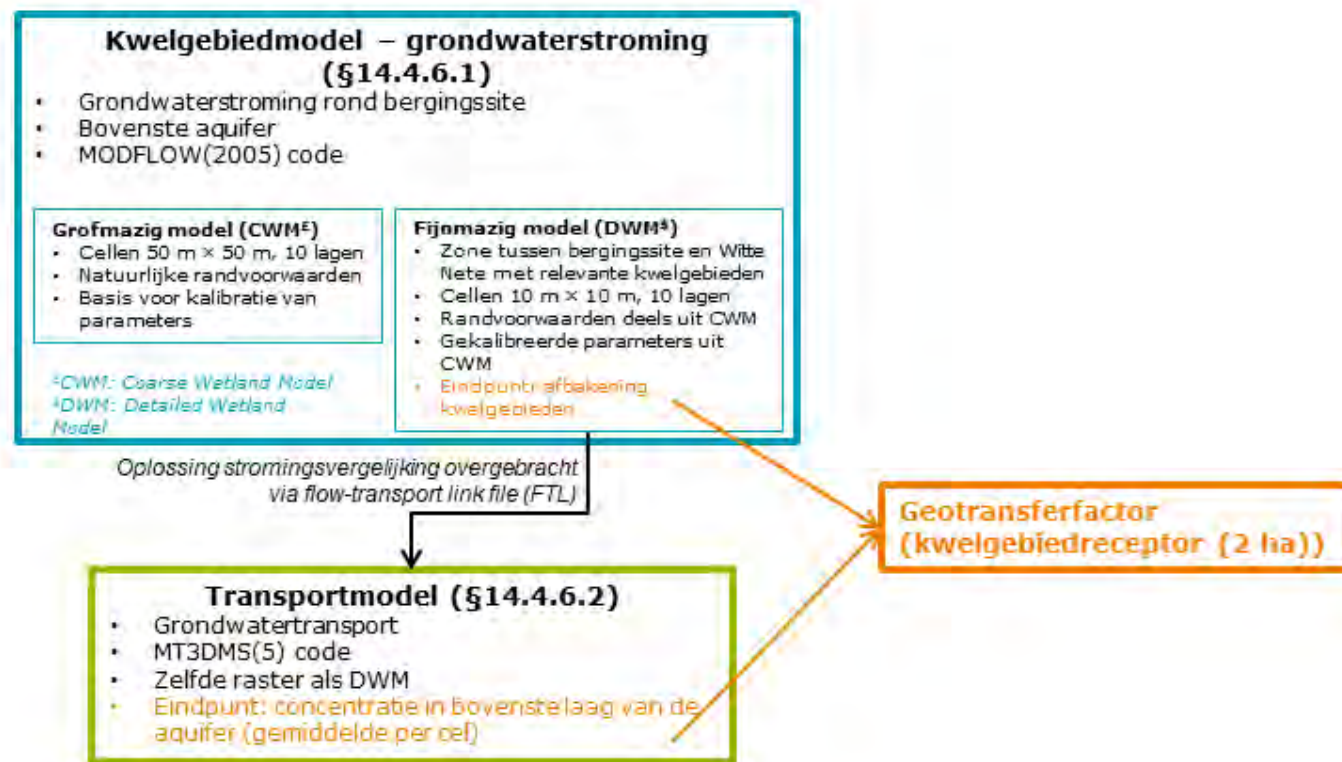
# Why different GTFs?

- GTF is calculated for different biosphere receptors:
  - Private well: at the most adverse location at the foot of the tumuli
  - Wetlands: areas where (contaminated) groundwater reaches the roots of plants and a RN transfer can take place
  - River: drainage of (contaminated) groundwater to river network



# How do we obtain GTFs?

- Hydrogeological modelling
  - Groundwater flow model
    - Often using nested models to combine the natural boundary conditions with need for precision
  - Groundwater transport model
    - Using results from the flow model
    - Simulating constant activity flux through disposal tumulus
    - RN independent



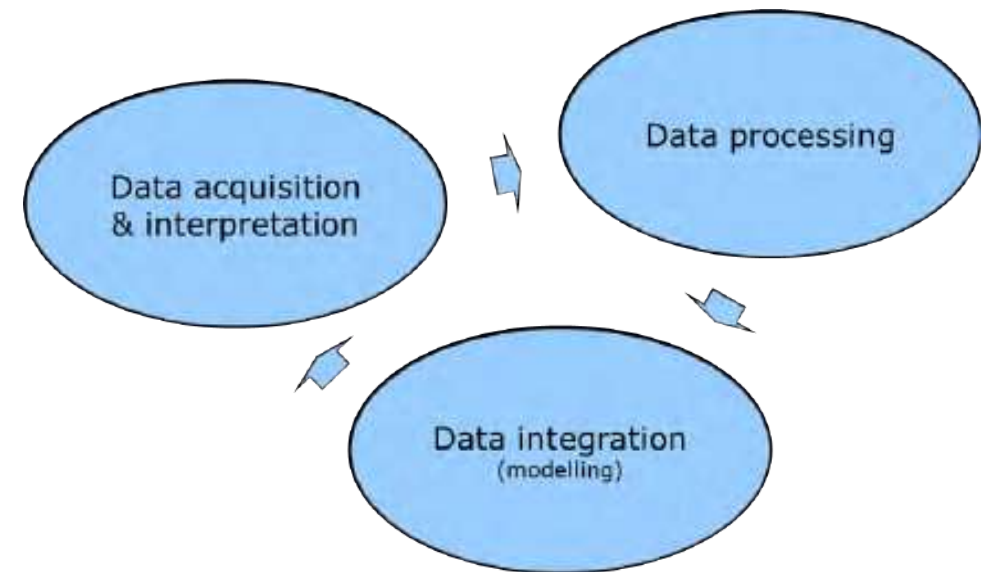
# KNOWING THE ENVIRONMENT





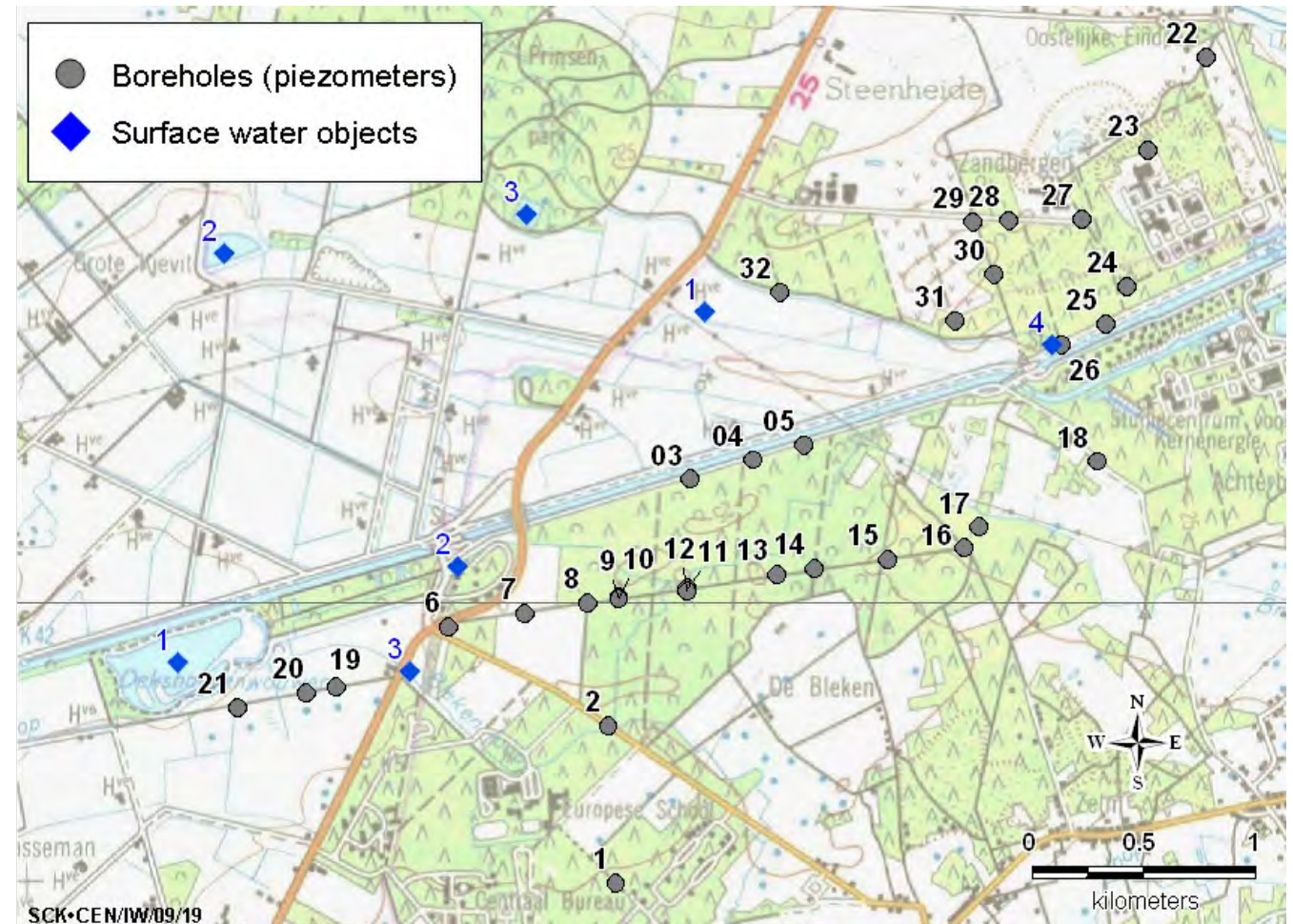
# The characterization of the environment

- Long-term: starting in 1999 and lasting to date
- Stepwise iterative approach
  - Every site characterization campaign is followed by modelling
  - Every modelling is evaluated & then reviewed by the Safety Authority
  - This leads to further characterization to answer the raised questions
- Gradually focusing the site-characterisation efforts on building a solid safety-relevant scientific basis



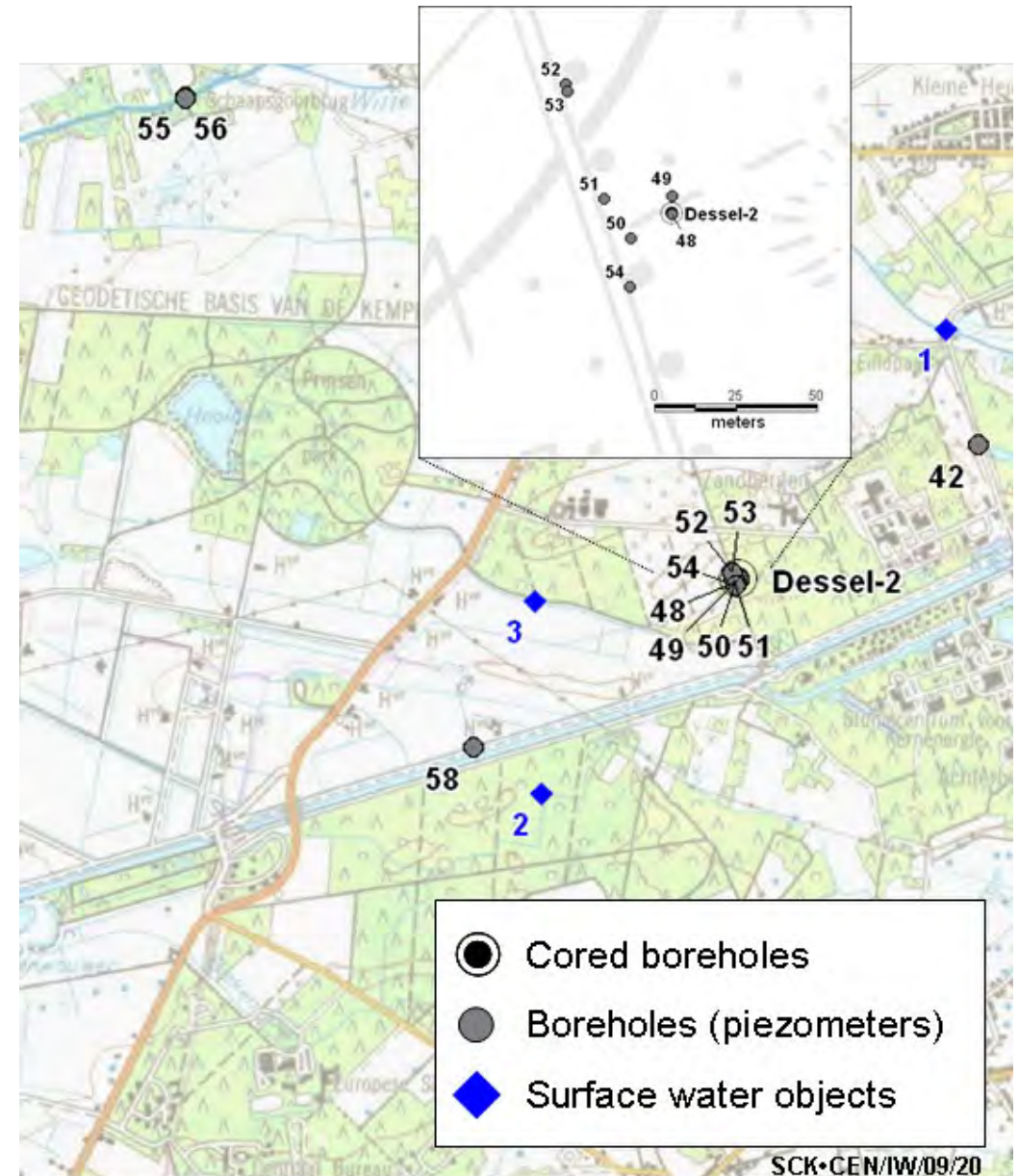
# Campaign 1999 – 2000

- Focused on piezometry and surface water level observations
- Basis for the local piezometric network
- One pumping test L-11
  - South of the canal
- Initial modelling
  - *Role of Kasterlee Clay?*
  - *Boundary conditions?*



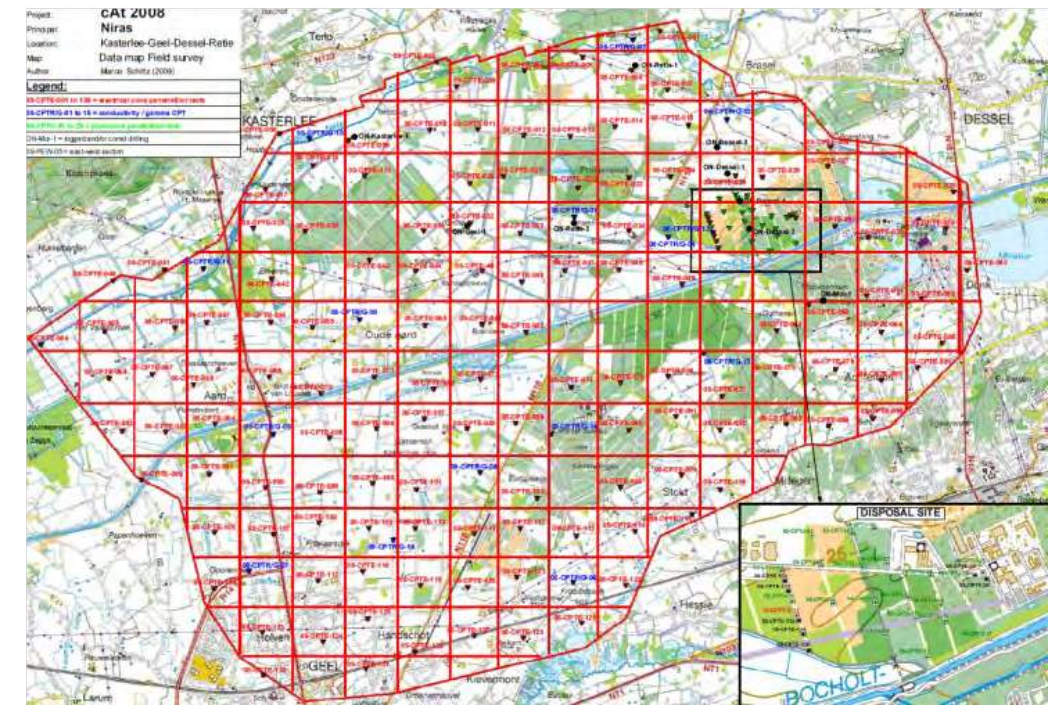
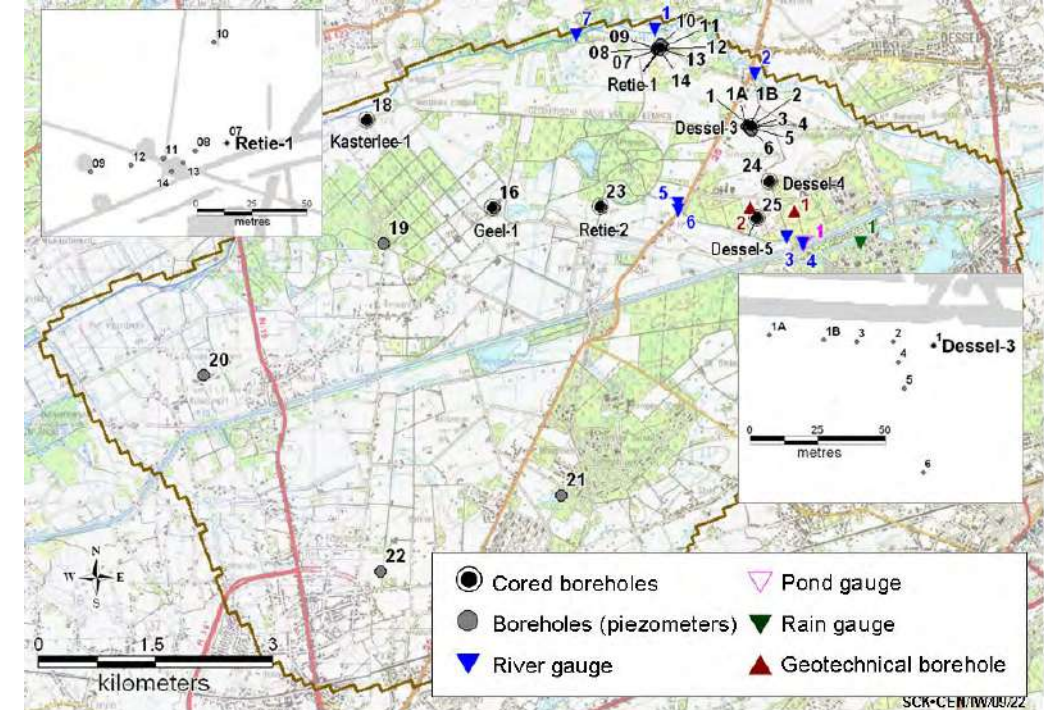
# Campaign 2002

- Focused on hydraulic parameters at the cAt site
- Verification of the Kasterlee Clay (im)permeability
- Dessel-2 borehole cluster
  - 2 pumping tests
  - Core sample analyses
- Few extra piezometers and surface observations points
  - Focused on the boundary conditions (Nete, Hooibeek, sand pit, canal)
- Local model 1<sup>st</sup> iteration:
  - *Is Kasterlee Clay (dis)continuous?*
  - *Spatial coverage of observations?*



# Campaign 2008

- Focus on the entire Local model area
- Filling the white spots
- Focus on the principal pathway
  - Piezometry
  - Pumping tests
  - Core sample analyses
- Kasterlee Clay continuity verification
  - **Cone Penetration Testing**
    - Performed on a regular grid
    - More precise stratigraphy
    - Detailed geometry of the Kasterlee Clay
- Local model 2<sup>nd</sup> iteration (SC 2013)
  - *Can we validate the flow direction and velocity?*



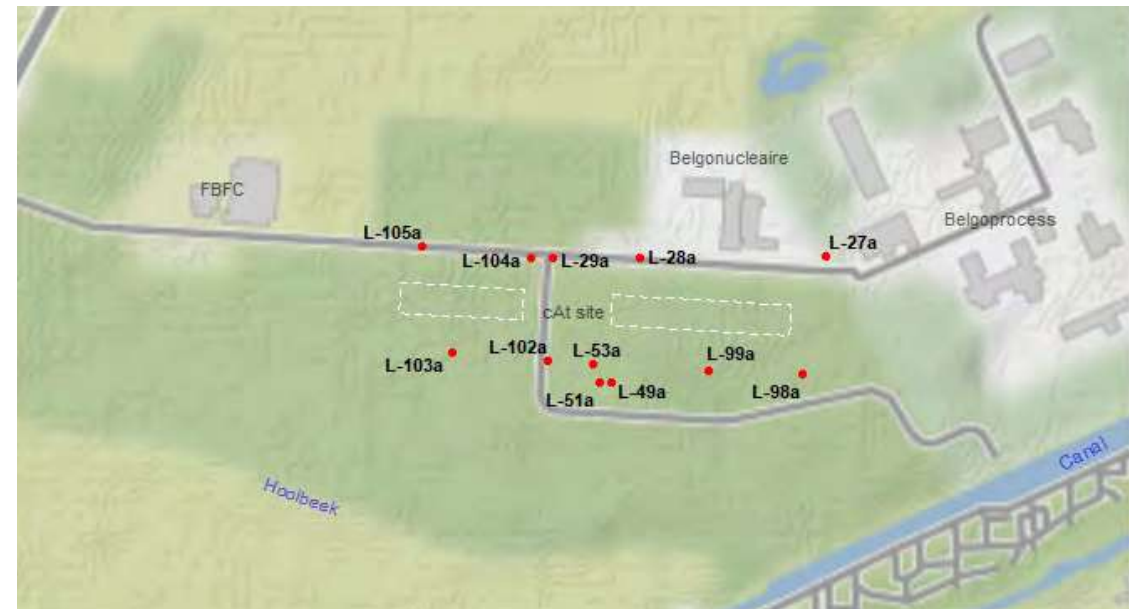
# Campaign 2016 – 2019

- Focused on validation of the flow direction and velocity
- New temporary piezometers at the cAt site
  - monthly measurements -> daily interpolated maps
  - summary plots for flow direction under the tumuli
- Dilution tests
  - Existing and new piezometers
    - Long filters and minimizing the excavation disturbed zone
- Answers to the Safety authority
  - *Steady-state flow confirmed for the eastern tumulus*

Water table mapping



Dilution tests



# GROUNDWATER MODELLING



# Three models

- Private well Eastern tumulus
  - Steady-state model
  - Approved in 2019
- Private well Western tumulus
  - Transient model
  - Unfortunately, insufficient data for validation (see further)
- Wetland Eastern tumulus
  - Transient model with more details in wetland areas
  - Approved in 2023

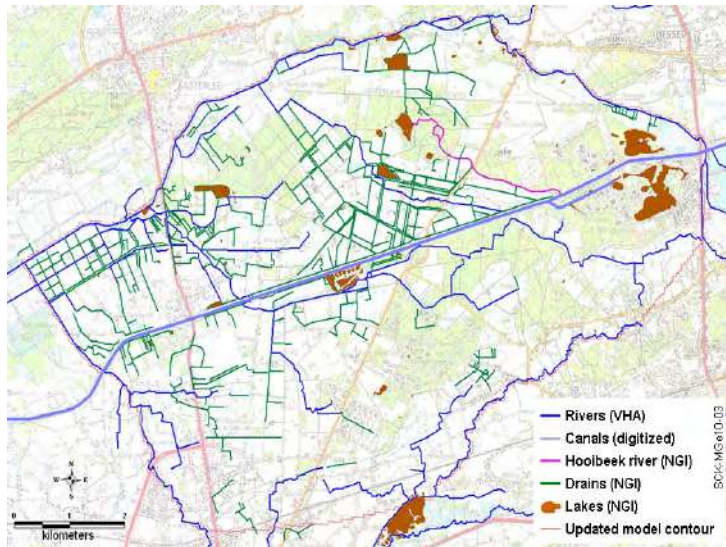




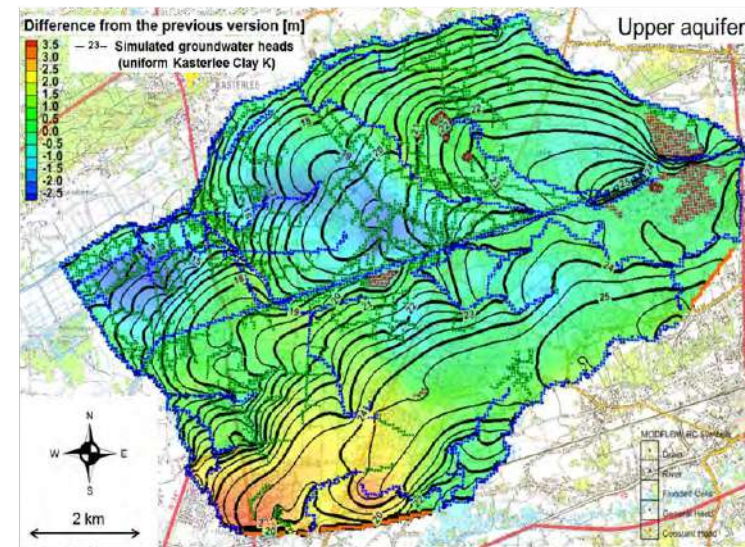
# Steady-state model – Local model (safety case 2013)

- Constant boundary conditions lead to time-invariant flow and velocity field

**Constant** recharge flux; river, lake, drain levels

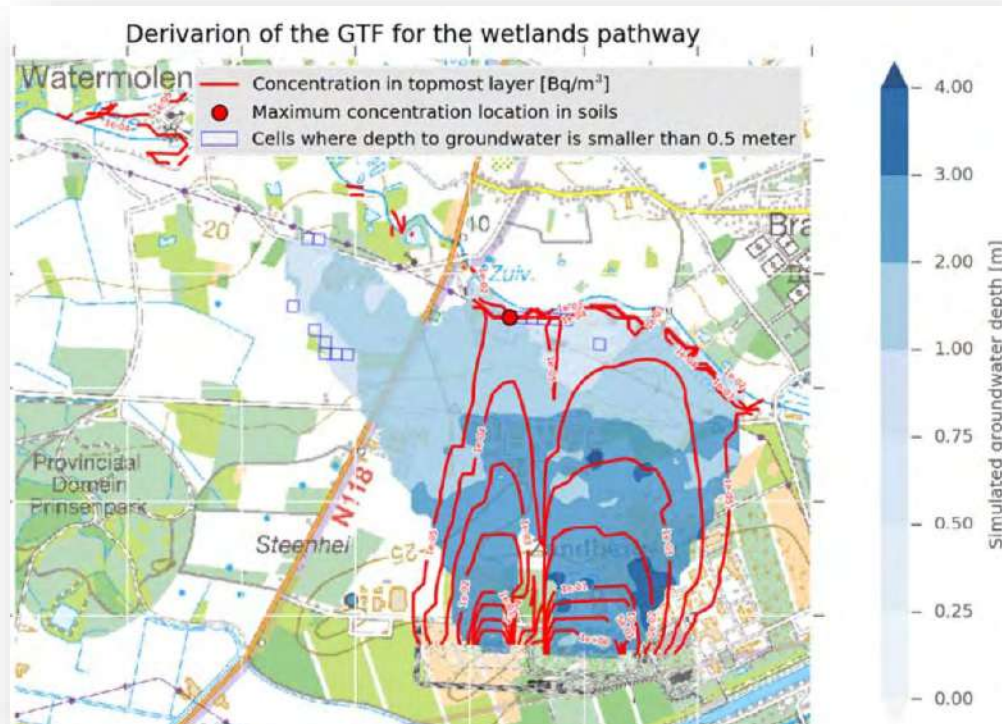


**Single** (equilibrium) flow-field representation



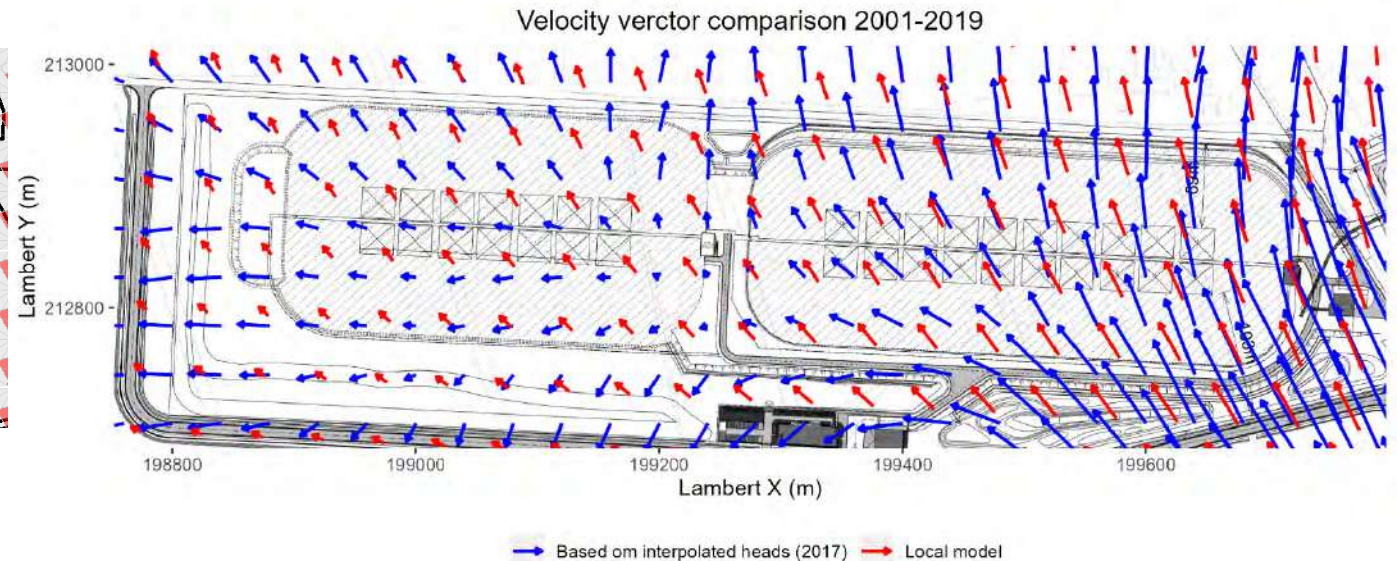
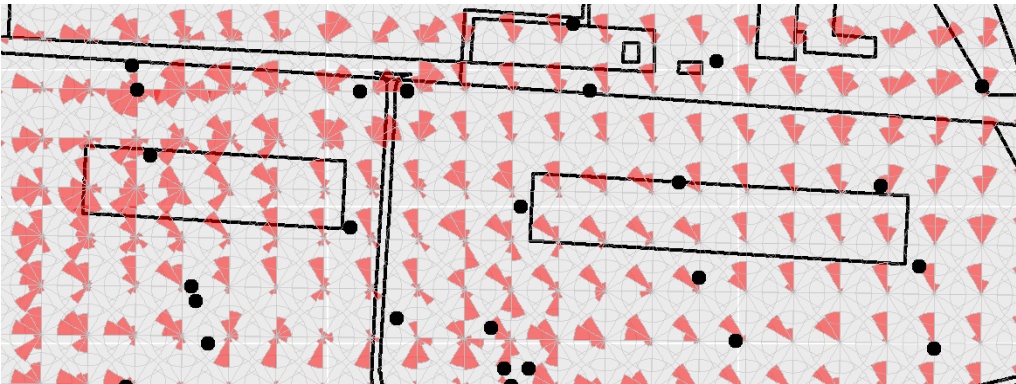
# GTFs calculated

- The GTF was calculated for three receptors:
  - Eastern tumulus private well ( $1.7 \times 10^{-5} \text{ a/m}^3$ )
  - Wetlands:  $4.7 \times 10^{-9} \text{ a/m}^3$  ( $\ll \ll \text{GTF}_{\text{well}}$ )
  - Rivers ( $\text{Flux}_{\text{rivers}} = \text{Flux}_{\text{source}}$ )



# Invariant flow field is validated (for Eastern tumulus)

- Comparison between the single model result and daily interpolated heads
  - Eastern tumulus: reasonable fit & low variability (steady-state OK!)
  - Western tumulus: poor fit due a.o. to high temporal (seasonal) variability

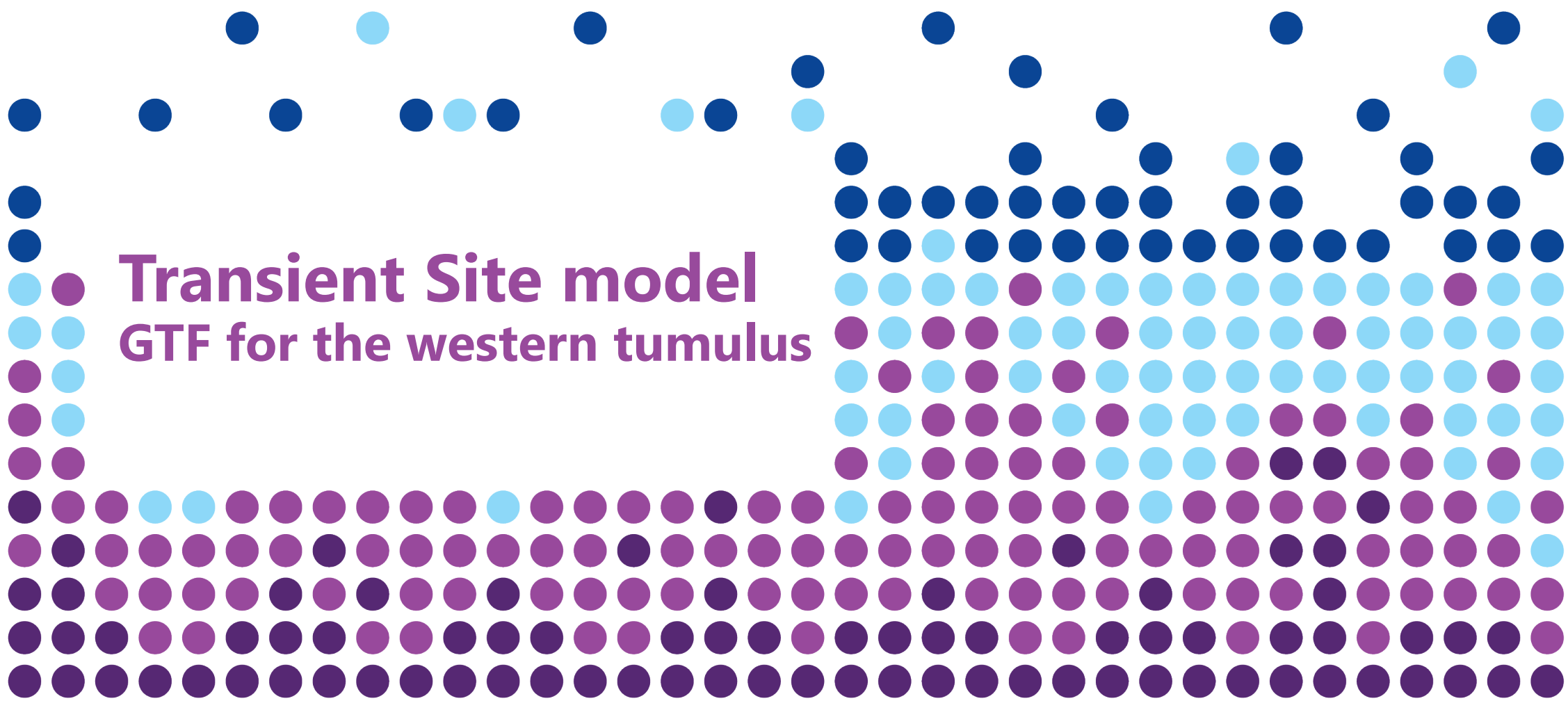


# Hence – the safety authority requested

- To confirm the hydrogeological at the Western tumulus based on field data
- To develop a new hydrogeological model that:
  - correctly describes the actual conditions at the disposal site and its surroundings
  - allows to provide conservative estimates of the GTF for the Western tumulus
- To validate the model for the identification of wetland areas and the estimation of dilution in the upper part of the aquifer (eastern & western tumulus)

# New data revealed the complex situation at the Western tumulus

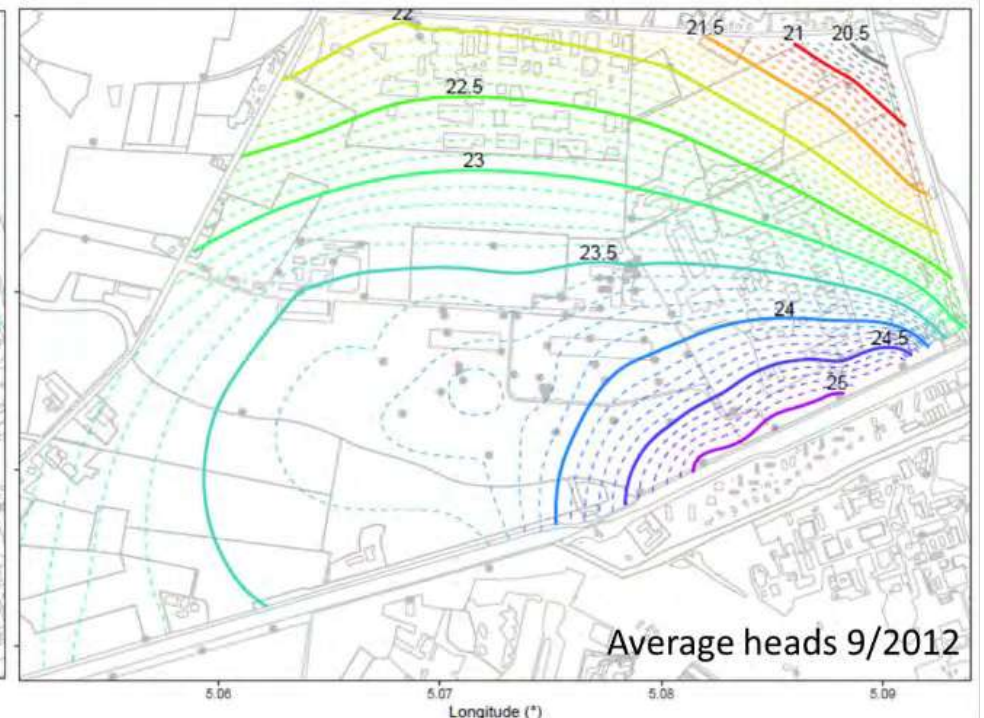
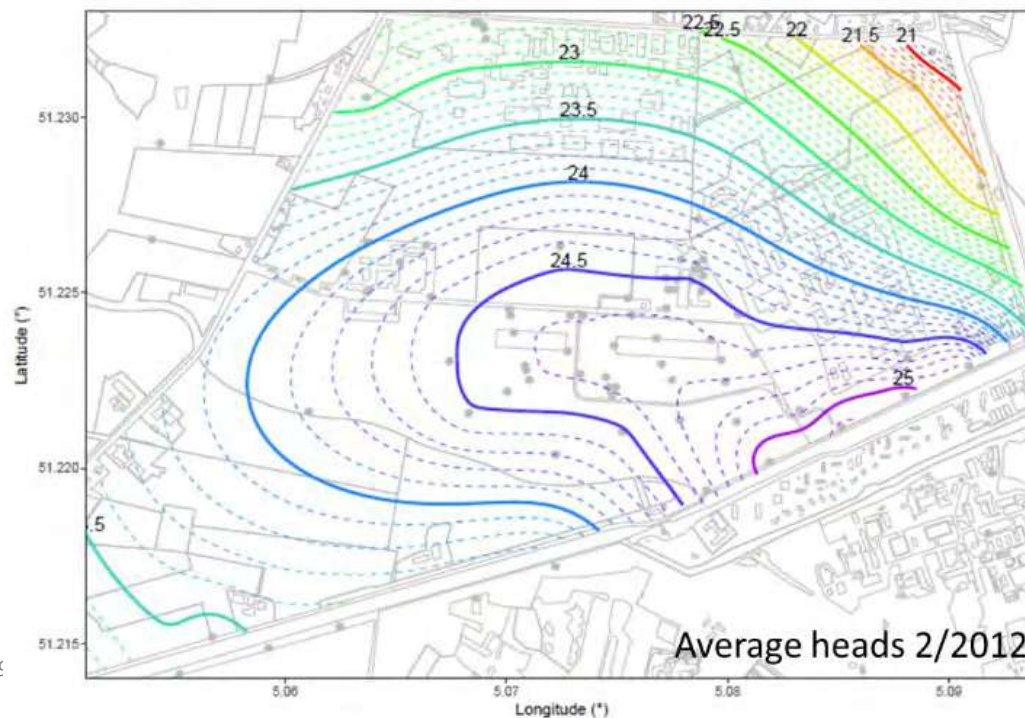
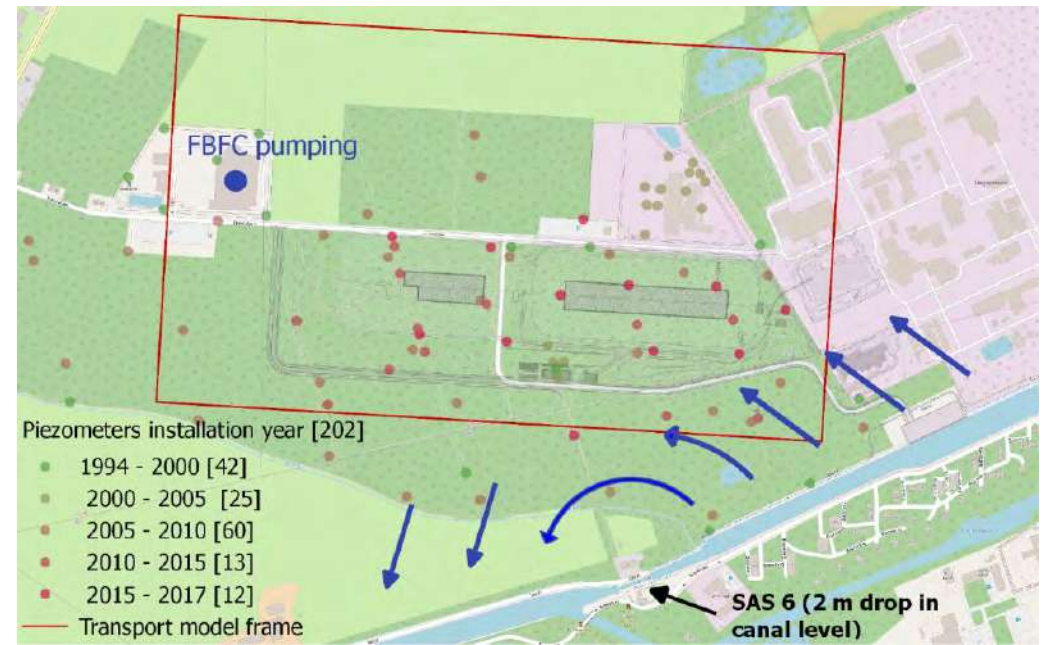
- New data (see before) and new statistical data analysis revealed that a steady-state model with invariant flow fields (and velocities) is not representative for the Western tumulus
- Therefore, a model with variable boundary conditions (recharge, river levels) is required.



**Transient Site model**  
**GTF for the western tumulus**

# Hydrogeology at the western tumulus

- Flat groundwater table
- Influenced by
  - the leaking canal
  - seasonal recharge
  - pumping operations



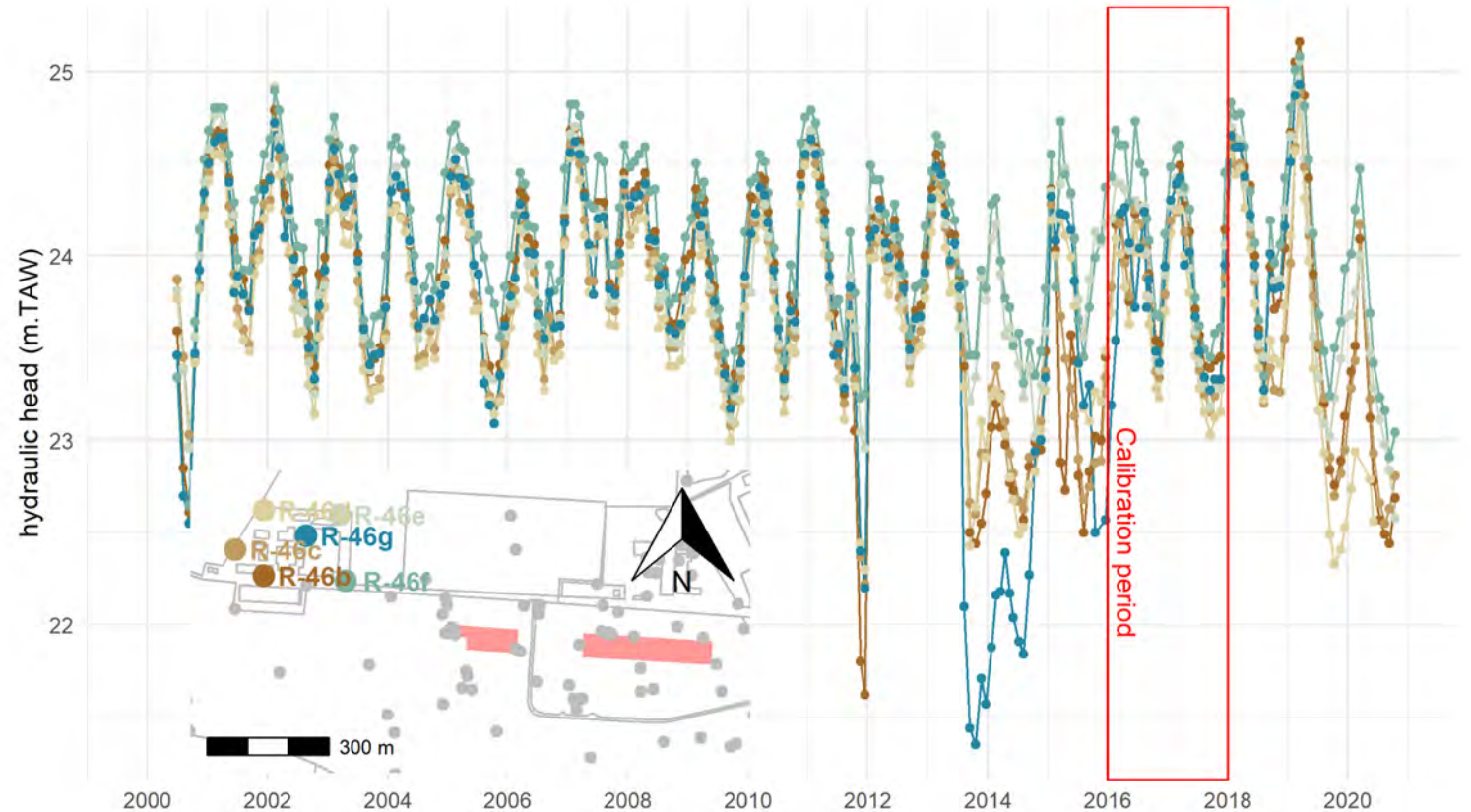
# Site model

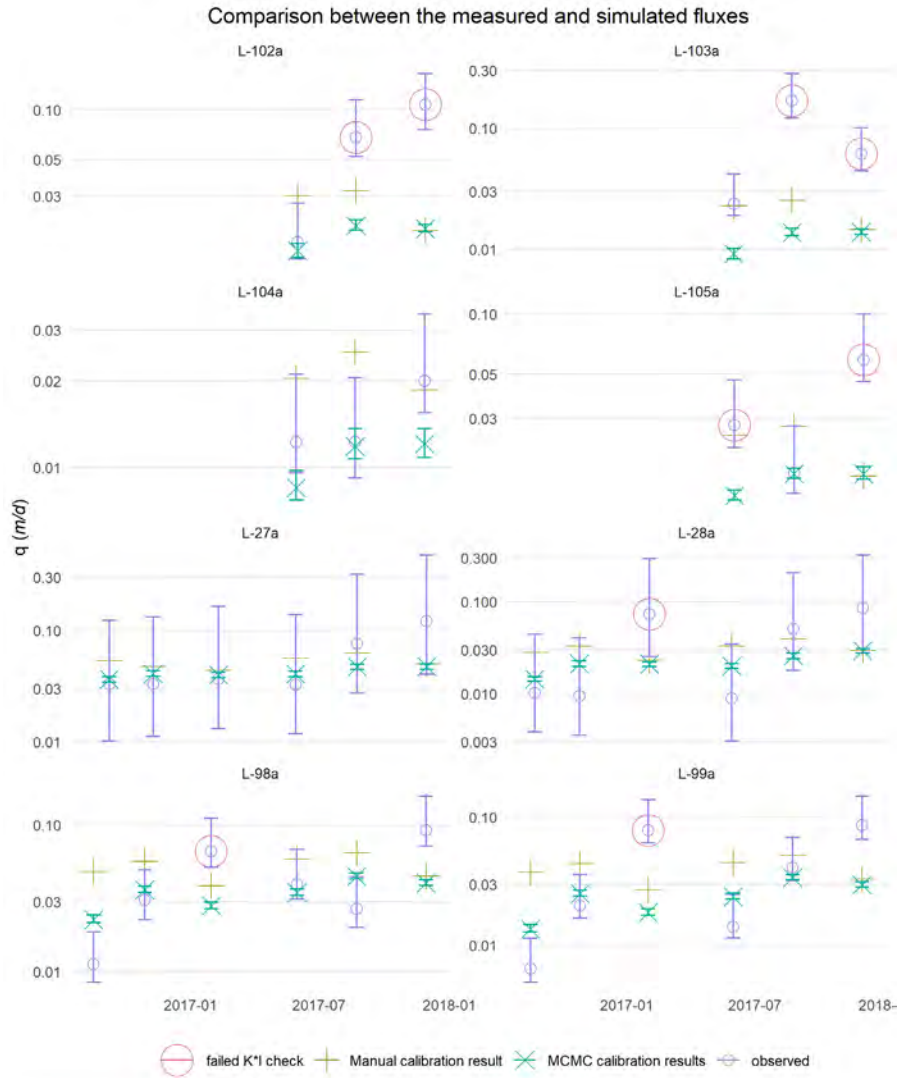
- Transient groundwater model
  - Extent focused on the upper aquifer
  - Grid refinement (child model) to increase the resolution of transport
  - Recharge dependent on transient precipitation, soil properties and land-use
  - Hydraulic parameters from site characterization and best knowledge



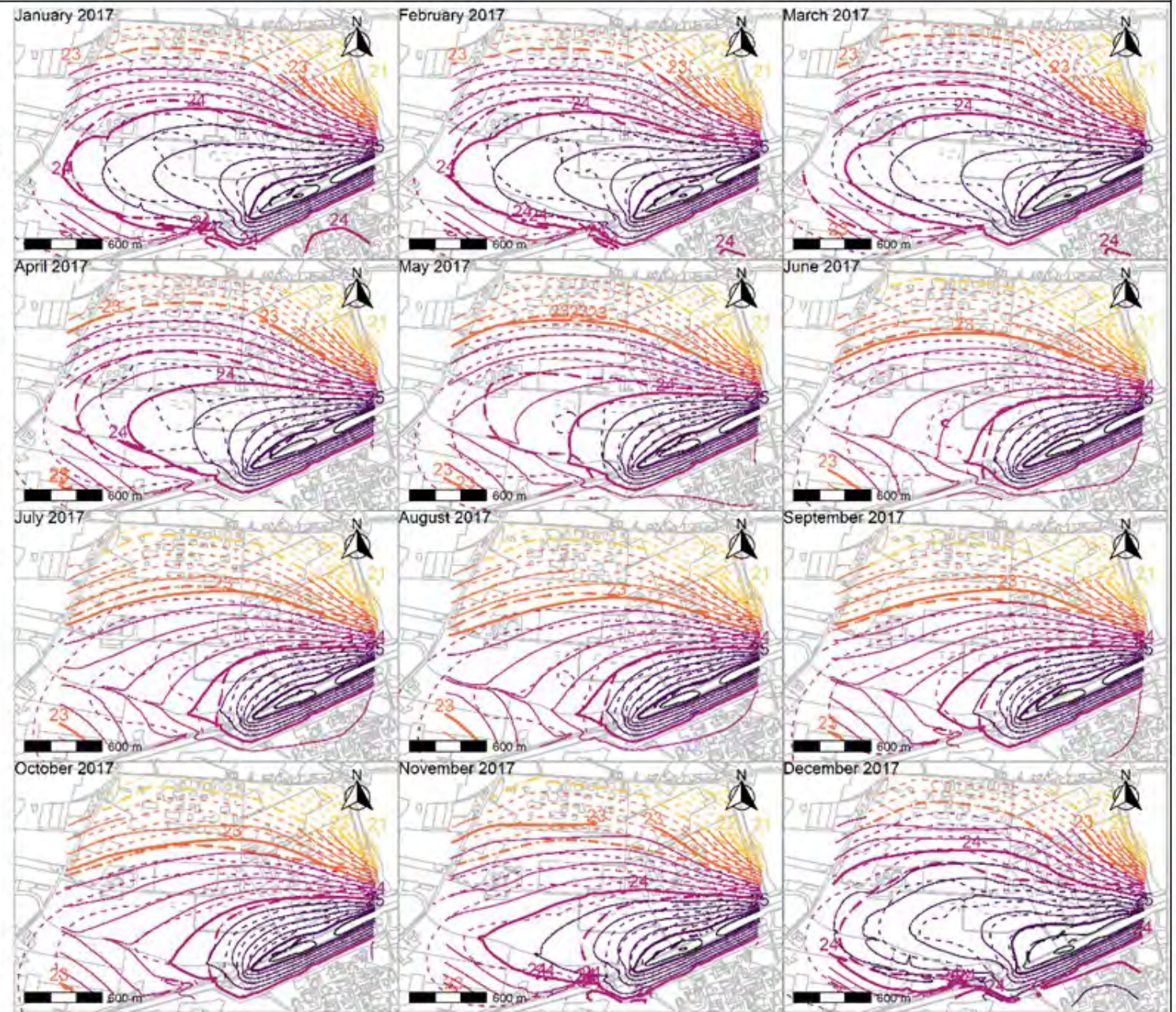
# Calibration

- Calibration using the observed heads and fluxes
- Selecting period with limited influence of pumping (at FBFC, BP, NIRAS cAt)
- Manual and automated calibration





Parameters calibrated using MCMC

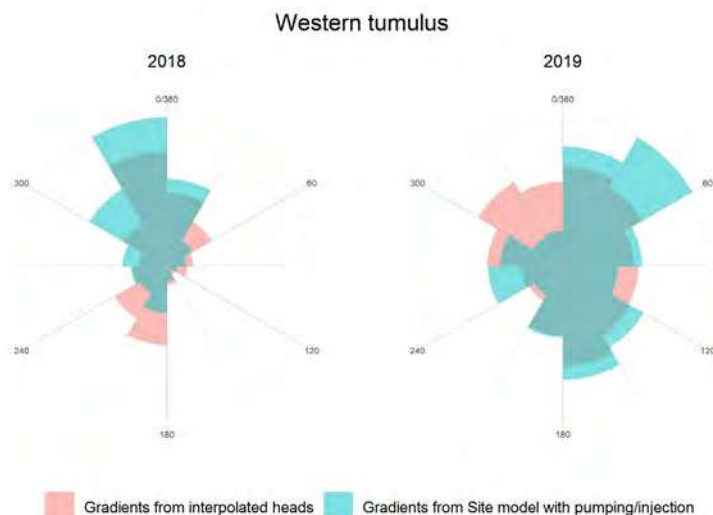


# Validation

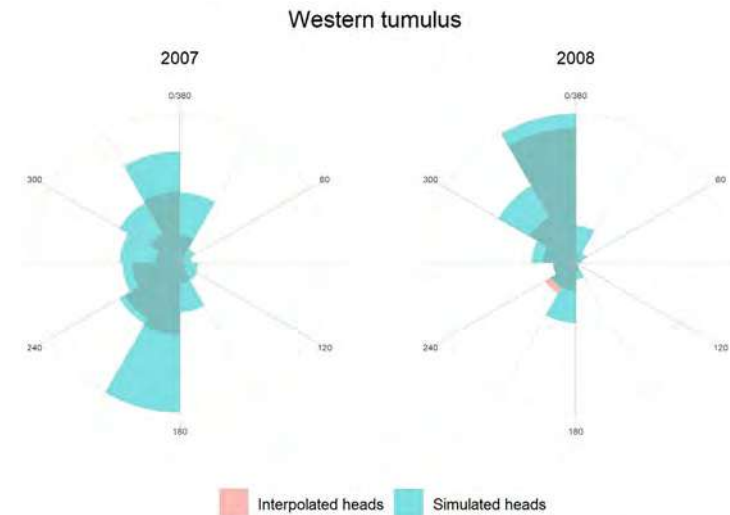
- Comparison of simulated with observed heads outside of the calibration period, turned out to be problematic, because:
  - The detailed observations period 2016 – 2019 influenced by pumping
  - Earlier periods not detailed enough
- Possibility to: either include pumping (no data available), or use less observations
- No good solution available...

## Comparison between the hydraulic gradients from interpolated maps and the model

With arbitrary pumping



Period with less detailed data



# Conclusions (Site model)

- The model cannot be satisfactorily validated
  - Need for a sufficiently long period of detailed observations without external influences (pumping)
- The GTF for the western tumulus cannot be calculated (for the moment...)
- Site characterization is entering a new phase:
  - Detailed piezometric measurements at the western tumulus using data loggers for a higher measurement frequency
  - Continuing the flux measurements



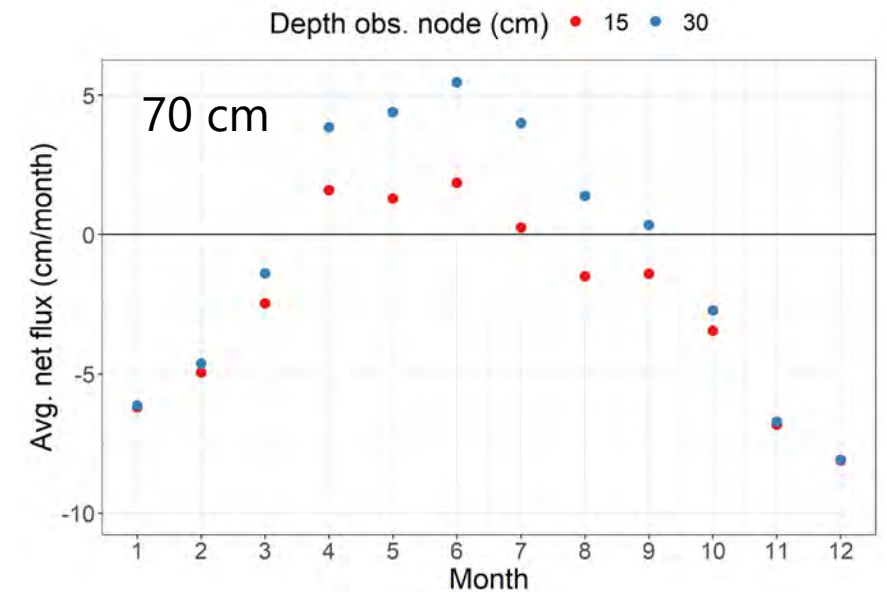
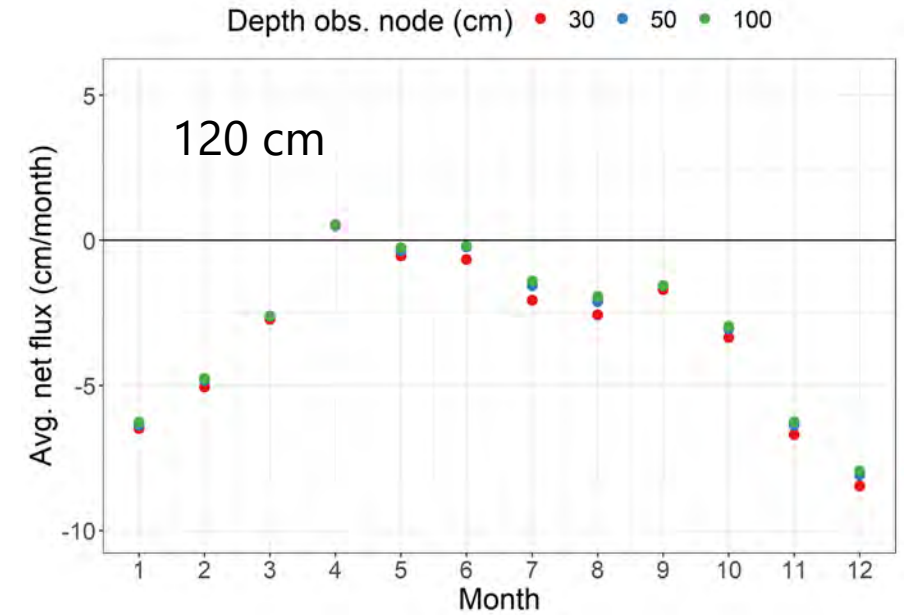
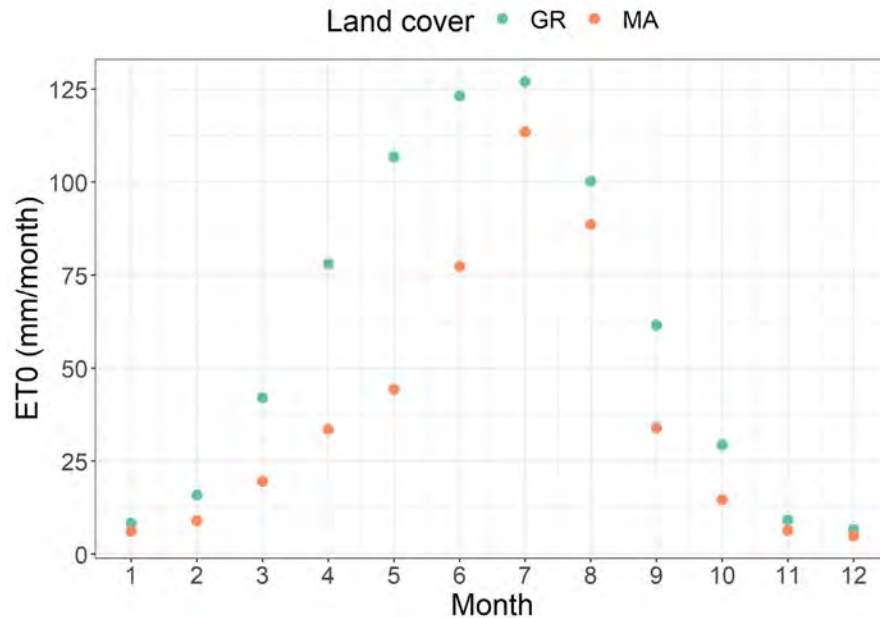
# Validation of the wetlands positions and GTF of wetlands

# But... what are “Wetlands”?

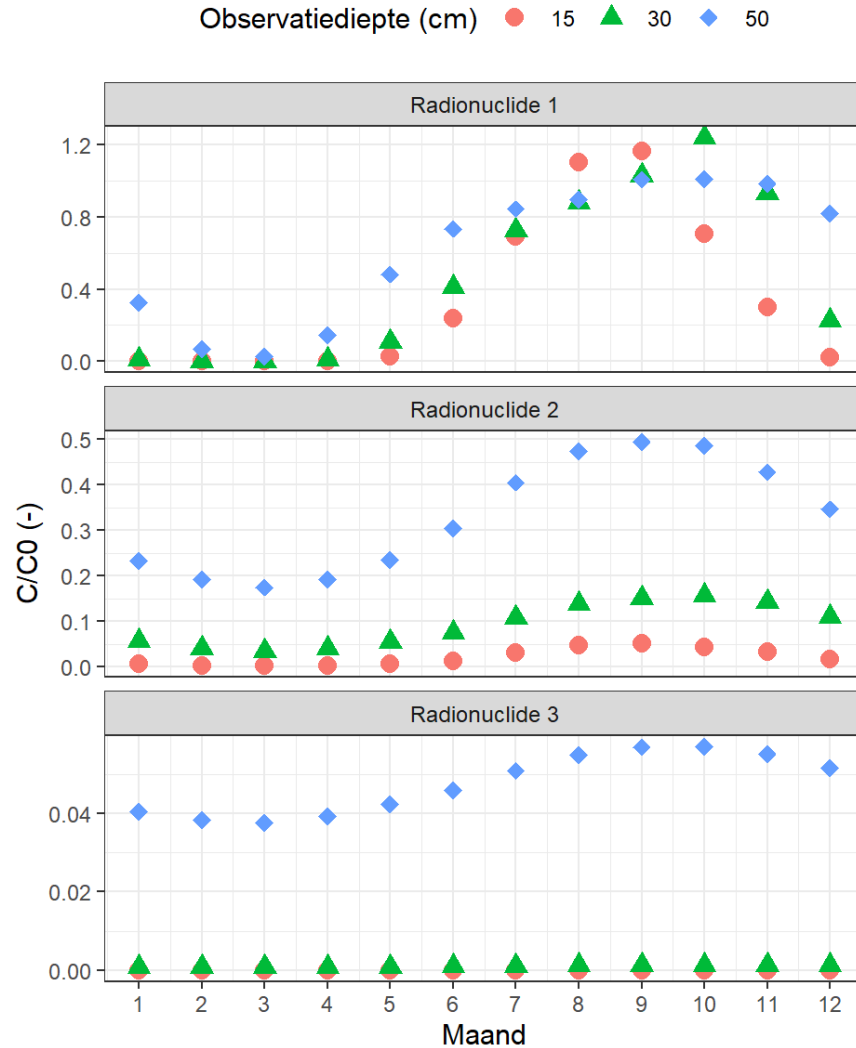
- Not in ecohydrological sense
- Entrance point of radionuclide in the soil and crop compartment (30 cm topsoil) via groundwater and upward fluxes

# Delineation criterium

- Transient model – time of highest groundwater level does not coincide with time of highest upward flux.



# Delineation criterion

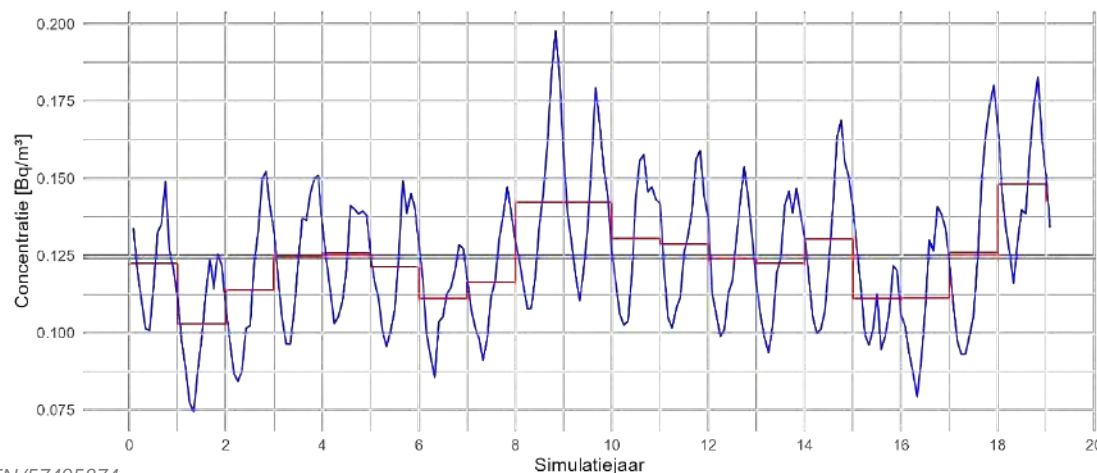


- Based on stylized scenarios: long-term average ground water level less than **70 cm** below surface in **April or May**.



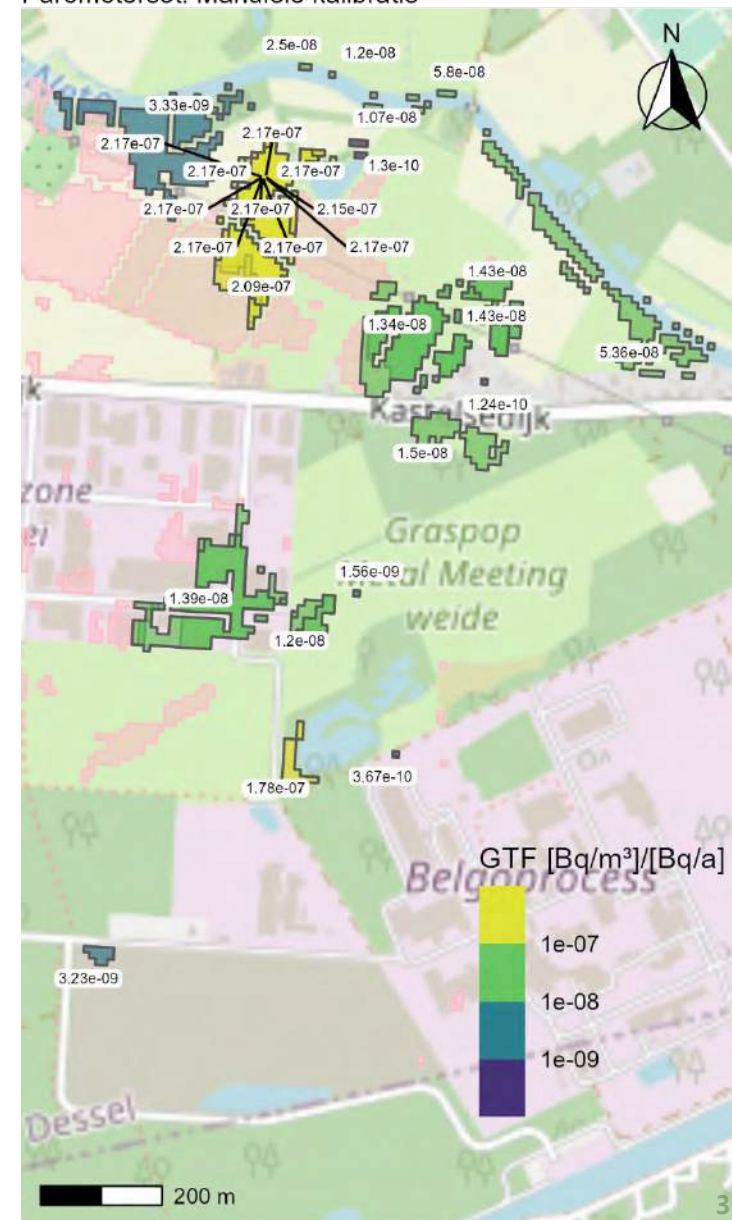
# Wetland receptor definition

- Wetland receptor is defined in several steps:
  1. Calculate the cell GTF
    - Based on long-term average concentration and source flux
  2. Overlay with map of wetlands
  3. Lookup all 2 ha areas (200 cells of 10×10 m) – potential wetland receptors
    - Selecting the highest value – wetland receptor



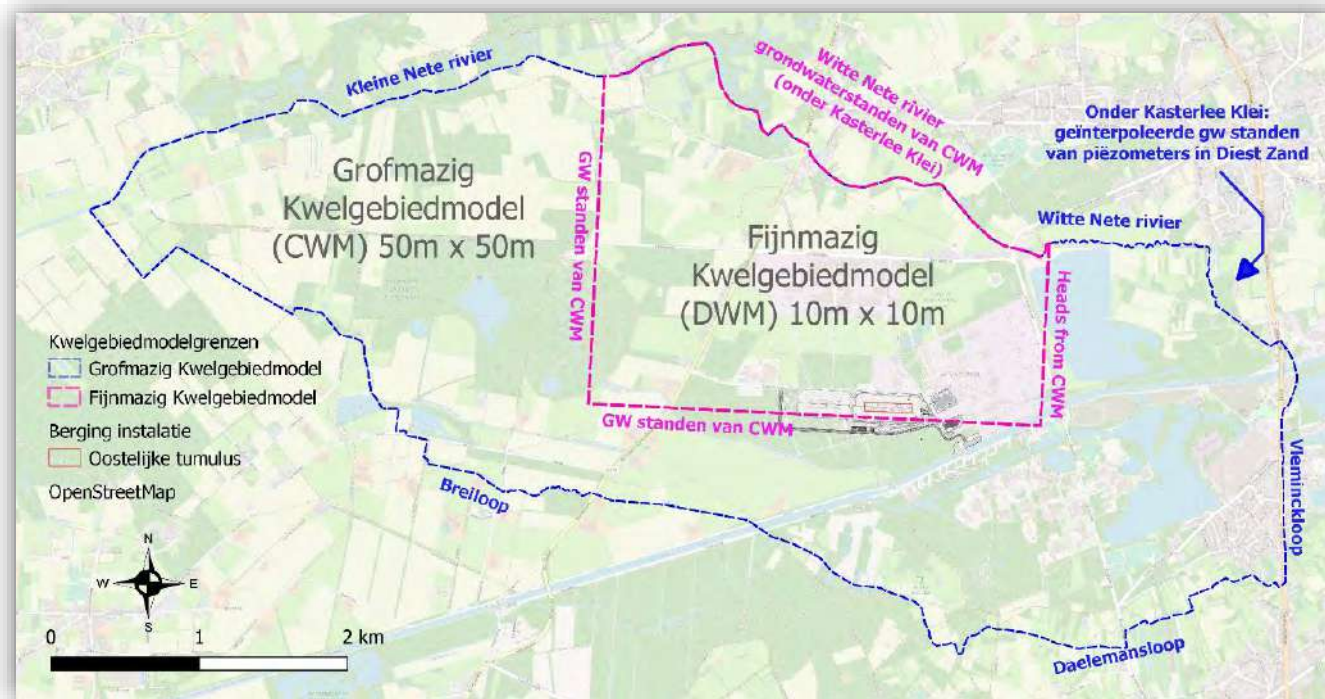
— Jaarlijkse concentratie — Lange-termijn concentratie — Maandelijkse concentratie

Klimaat: CCI HYDR hoog/nat  
Landgebruik: uniforme gras  
Concept: geen kanaal & hooibeek  
Parameterset: Manulele kalibratie



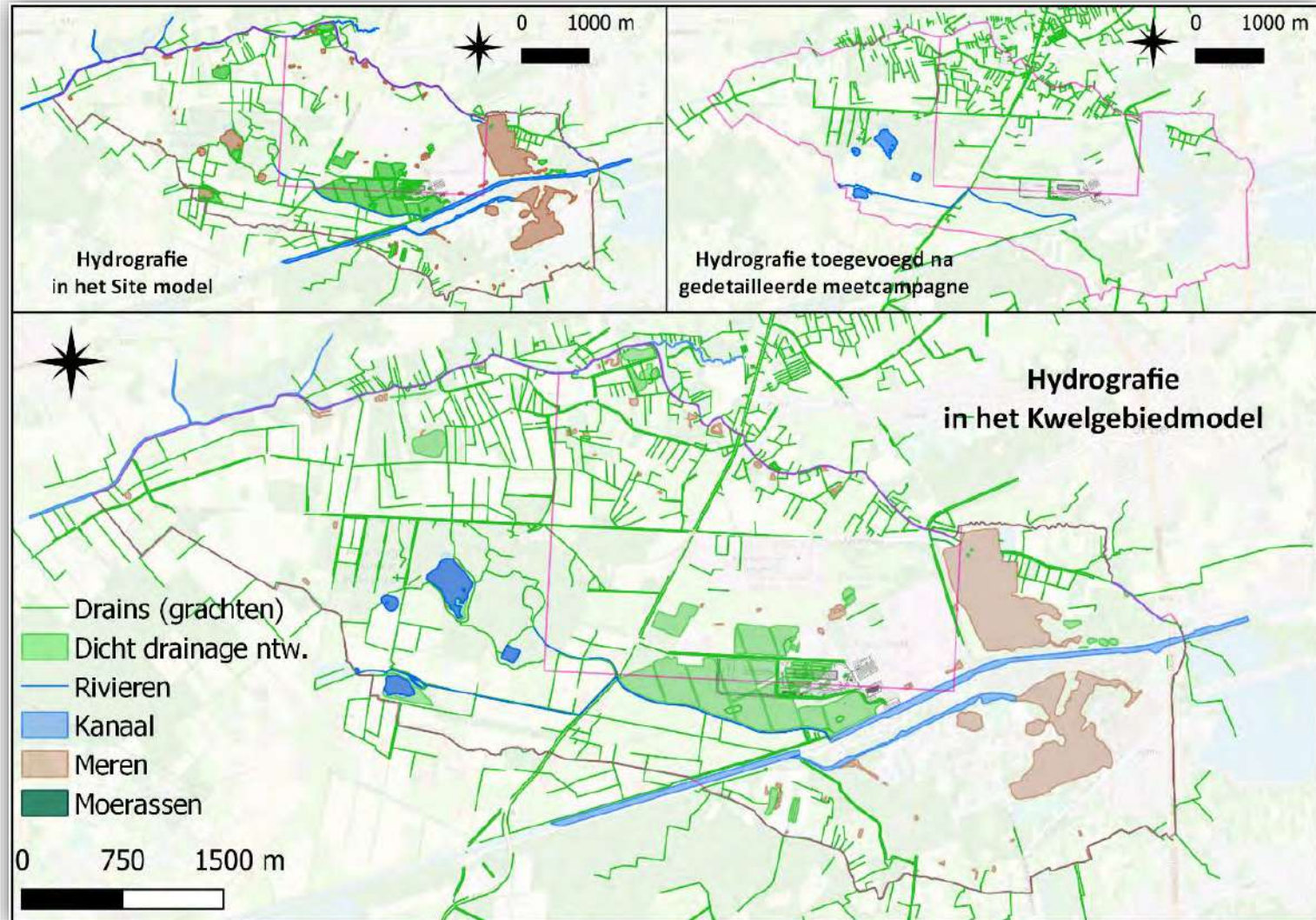
# Building the flow model for the wetlands

- Largely based on the Site model:
  - Extent of the parent (coarse) model
  - Hydraulic parameters
  - Recharge
- Different focus:
  - Pathways of RN from the Eastern tumulus
  - Not in the immediate vicinity of the disposal site (relatively deep groundwater level)
  - Hydrology important, especially in the agricultural zone close to Nete River level dynamics



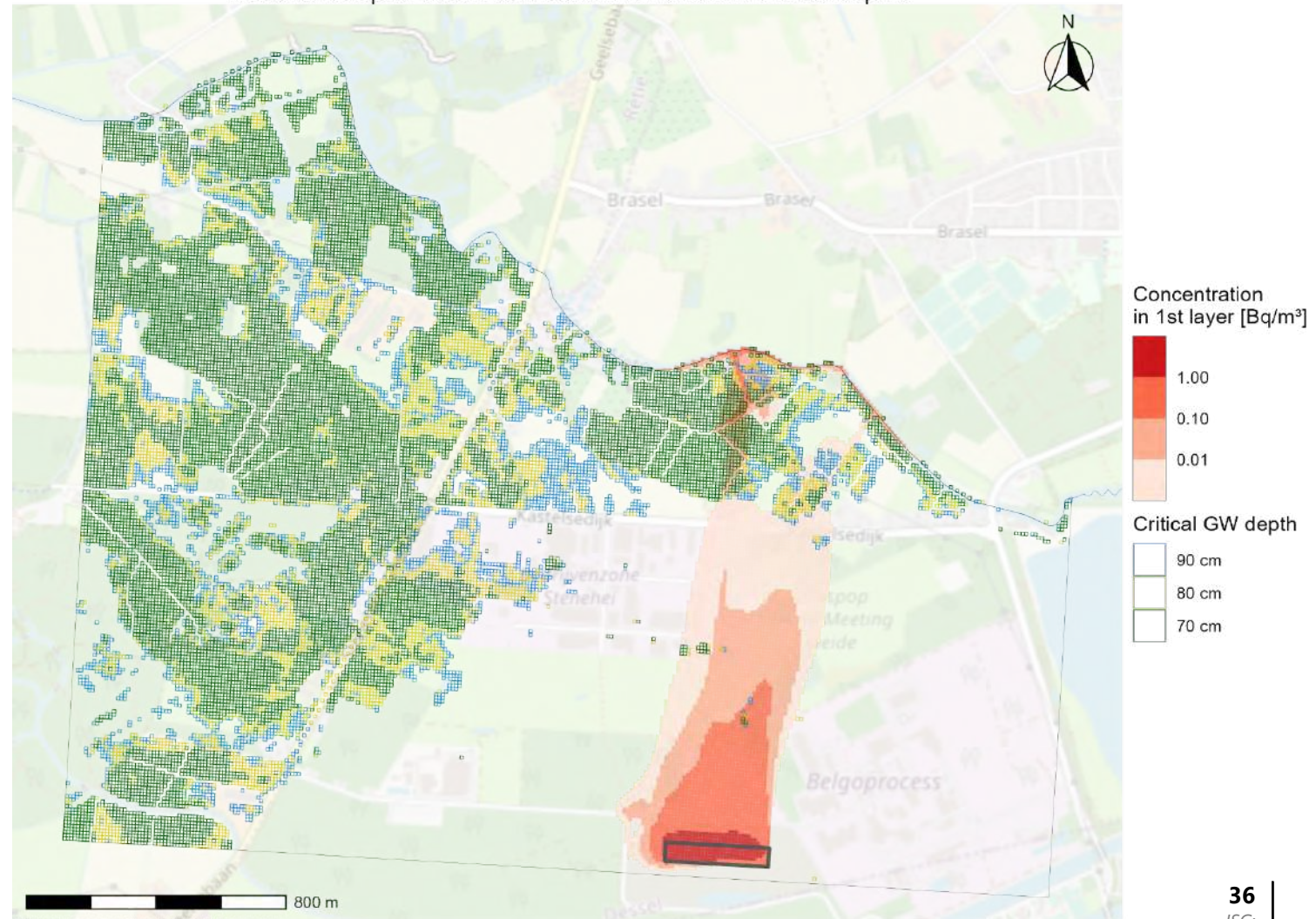
# Wetland model detailed hydrography

- Field survey (IMDC)
- Mapping & measuring the levels
- River hydraulic modelling
- dynamic river stages



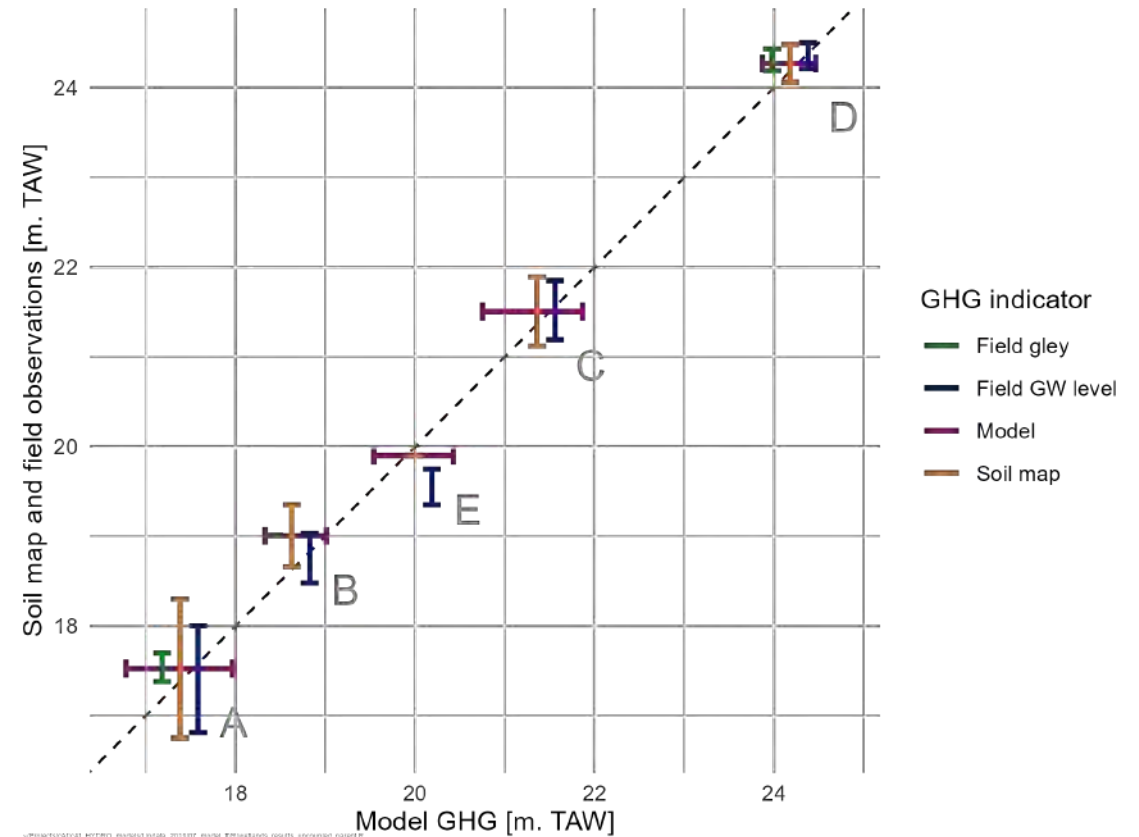
# Wetland delineation

Wetland receptor extent delineation for different critical depths



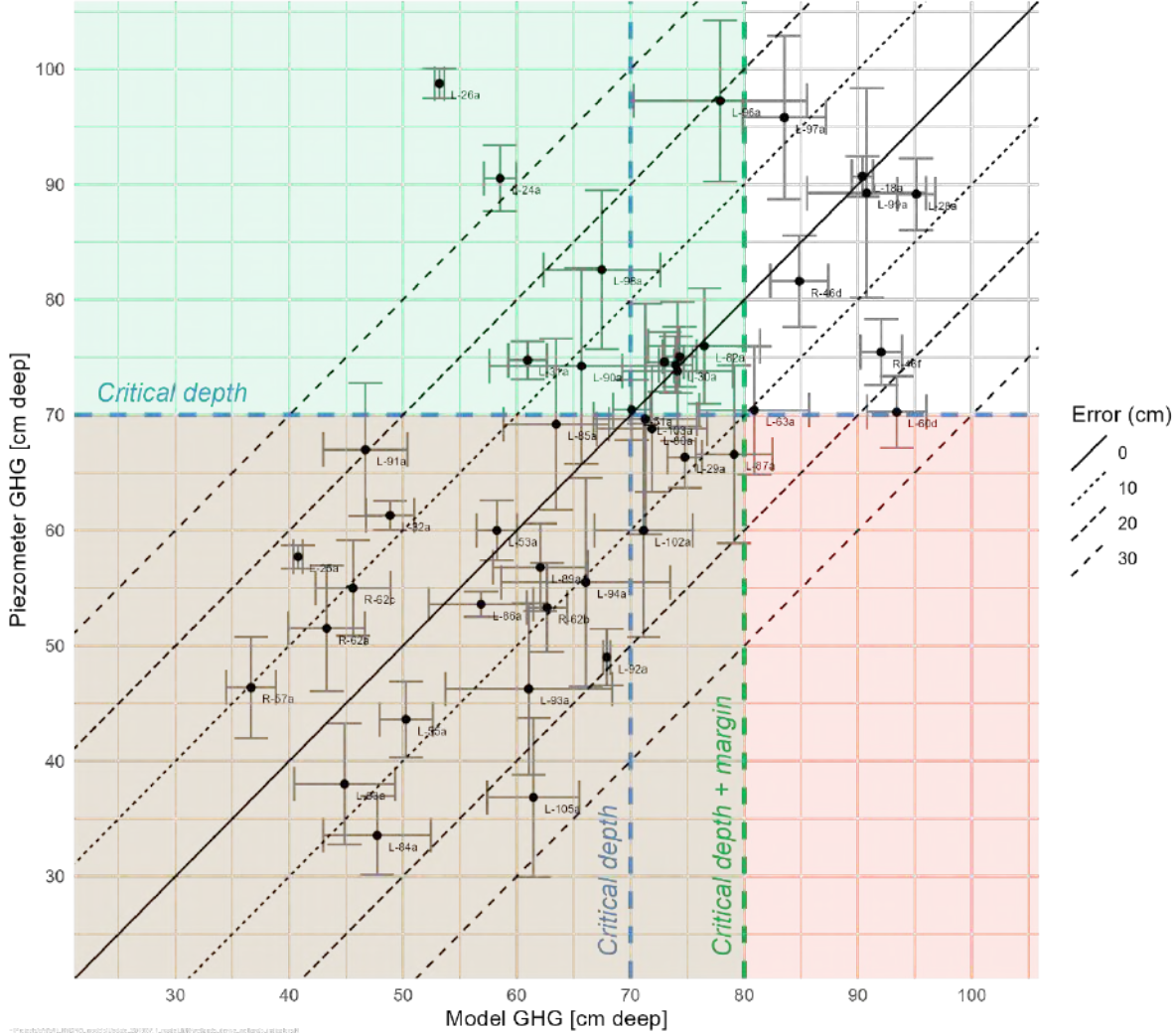
# Validation of Wetland locations

## Soil map information and field work



# Validation of Wetland locations

## Averaged groundwater levels



# Towards a conservative estimate of the GTF

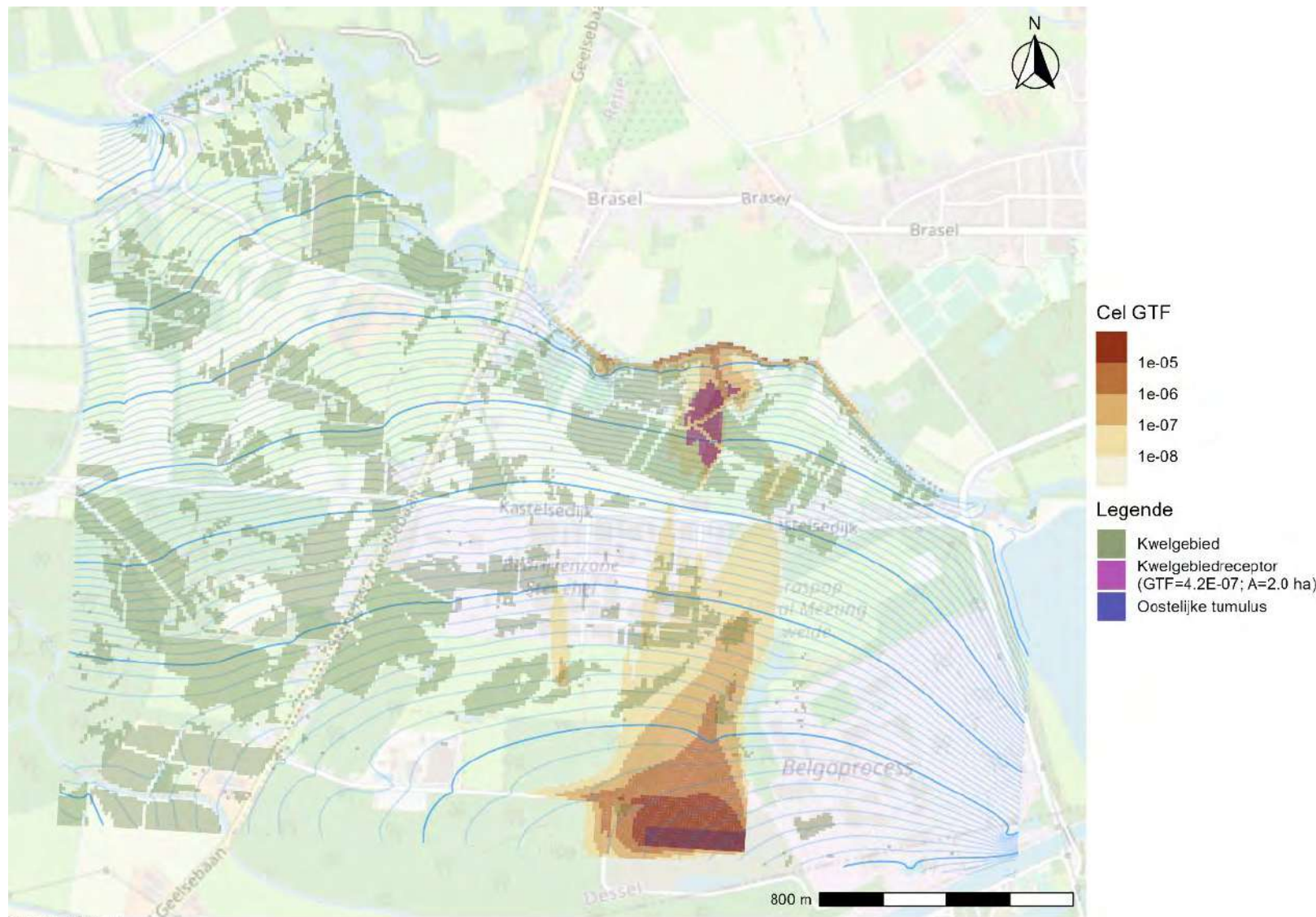
# Consideration of possible future changes

- Step-wise approach
  - Variant 0 – application of the reference future climate on current land-use
  - Variant 1 – model adapted for the future climate simulations
    - Recharge excess eliminated: solved by in an iterative procedure
  - Reference variant – stylized model using a number of assumptions:
    - Uniform land-use
    - Reference climate scenario
    - Presence of the canal
    - Parameter set
  - GTF sensitivity:
    - Consequences of alternative choices & scenarios



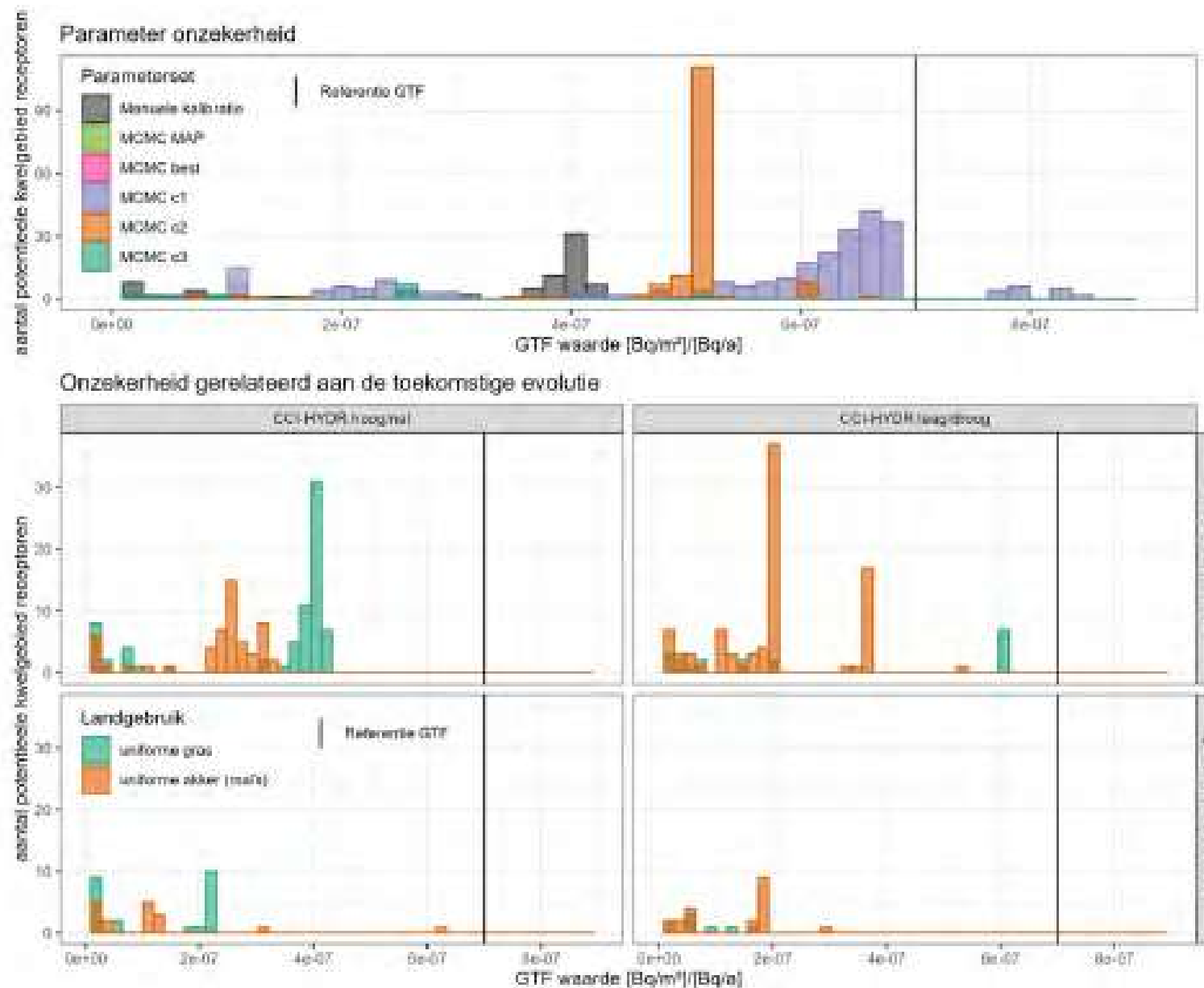
# Results: reference variant

- Reference variant:
  - CCI-HYDR high/wet climate
  - Manually calibrated parameters
  - Uniform grass land-use
  - Canal exists
- $GTF = 4.2 \times 10^{-7} \text{ a/m}^3$



# GTF sensitivity & selection of the reference GTF

- Reference  $GTF_{wetl} = 7 \times 10^{-7} \text{ a/m}^3$



# Conclusions

- New hydrogeological model based on newest field measurements
- Validation of the model for:
  - the delineation of wetlands in the environment of the disposal site
  - the estimation of the dilution in the uppermost aquifer
- New & higher (larger impact) GTF for the wetland receptor
- **Confirmation** – radiological impact for private well receptor is the highest



# Conclusions & Future work

# Conclusion

- Eastern tumulus
  - Private well receptor – steady-state flow model approach
  - Wetland receptor
    - Detailed model in the area of wetlands
    - Transient flow model
- Western tumulus – Private well receptor
  - Detailed model in the area of the disposal facility
  - Transient flow model
- Model calibration OK
- Model validation – lack to sufficient high-quality data

# Future work - Continuous monitoring

- Extended and more in-depth monitoring of the area surrounding the Western tumulus
  - Coverage
  - More permanent structures
  - DAQ
  - Reducing the error
- Further monitoring of Eastern tumulus
  - Associated with the exploitation phase of the disposal facility
  - Radiological and chemical conditions in the vicinity of the disposal facility to detect any abnormal situation

# Future work - Modelling work

- Validated model (Site model) for Western tumulus based on the new data
- Confirmation of GTF values used in the safety assessment

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